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Optimal Source Distribution for Multiple Listener Virtual Sound Imaging

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3D sound with loudspeakers

B.B. Bauer, Stereophonic earphones and binaural loudspeakers, J. Audio Eng. Soc. 9 (2) (1961) 148-151.

B.S. Atal, M.R. Schroeder, United States Patent 3,236,949A, Apparent sound source translator, 1966.

P. Damaske, Head-related two-channel stereophony with loudspeaker reproduction, J. Acoust. Soc. Am. 50 (4B) (1971) 1109–1115.

Y. Ando, S. Shidara, Z. Maekawa, K. Kido, Some basic studies on the acoustic design of room by computer, J. Acoust. Soc. Japan 29 (1973).

S. Sakamoto, T. Gotoh, T. Kogure, M. Shimbo, A. Clegg, Controlling soundimage localisation in stereophonic reproduction, J. Audio Eng. Soc. 29 (11) (1981) 794-799.

H. Hamada, Construction of orthosterophonic system for the purposes of quasiinsitu recording and reproduction, J. Acoust. Soc. Am. 39 (5) (1983) 337-348.

J.L. Bauck, D.H. Cooper, Generalised transaural stereo and applications, J. Audio Eng. Soc. 44 (9) (1996) 683-705.

See also E.C. Hamdan. Theoretical Advances in Multichannel Crosstalk Cancellation Systems . PhD Thesis University of Southampton (2020)





Crosstalk cancellation for 3D sound









Block diagram





The half wavelength problem





Two source single listener geometry



$$\mathbf{d}^{\mathrm{T}} = \begin{bmatrix} d_{R} & d_{L} \end{bmatrix}, \ \mathbf{v}^{\mathrm{T}} = \begin{bmatrix} v_{R} & v_{L} \end{bmatrix}, \ \mathbf{w}^{\mathrm{T}} = \begin{bmatrix} w_{R} & w_{L} \end{bmatrix}$$
$$\mathbf{H} = \begin{bmatrix} H_{11} & H_{12} \\ H_{21} & H_{22} \end{bmatrix}, \ \mathbf{C} = \begin{bmatrix} C_{11} & C_{12} \\ C_{21} & C_{22} \end{bmatrix}$$
$$\mathbf{v} = \mathbf{H} \mathbf{d} \qquad \mathbf{w} = \mathbf{C} \mathbf{H} \mathbf{d}$$



Solution for the inverse filter matrix



$$\mathbf{C} = \frac{\rho_0 e^{-jkl_1}}{4\pi l_1} \begin{bmatrix} 1 & ge^{-jk\Delta l} \\ ge^{-jk\Delta l} & 1 \end{bmatrix}$$
$$g = l_1/l_2 \qquad \Delta l = l_2 - l_1$$
$$\mathbf{d}^{\mathrm{T}} = \frac{\rho_0 e^{-jkl_1}}{4\pi l_1} \begin{bmatrix} d_R & d_L \end{bmatrix}$$
$$\Delta l = \Delta r \sin\theta \text{ when } l \gg \Delta r$$
$$\mathbf{H} = \frac{1}{1 - g^2 e^{-2jkr\sin\theta}} \begin{bmatrix} 1 & -ge^{-jk\Delta r\sin\theta} \\ -ge^{-jk\Delta r\sin\theta} & 1 \end{bmatrix}$$



Singular values



Singular values of transmission path matrix become equal when

$$k\Delta rsin\theta = \frac{n\pi}{2}$$
$$\Delta l = n\lambda/4$$

 $n = \pm 1, \pm 3, \pm 5, \dots$



Takeuchi and Nelson JASA 112 (6) 2786-2797



Optimal source angle





11

Discrete approximation to the optimal source angle





Subjective experiments

• Azimuth localisation from 3-way discrete optimal source distribution (OSD)







Some OSD adopters





Sharp 8A-C22CX1





Sherwood S7



Three Channel Optimal Source Distribution



$$\mathbf{v}^{\mathrm{T}} = \begin{bmatrix} v_R & v_C & v_L \end{bmatrix}$$

$$\mathbf{H} = \begin{bmatrix} H_{11} & H_{12} \\ H_{21} & H_{22} \\ H_{31} & H_{32} \end{bmatrix}, \ \mathbf{C} = \begin{bmatrix} C_{11} & C_{12} & C_{13} \\ C_{21} & C_{22} & C_{23} \end{bmatrix}$$

$$\mathbf{C} = \frac{\rho_0}{4\pi} \begin{bmatrix} \frac{e^{-jkl_1}}{l_1} & s\frac{e^{-jkl_3}}{l_3} & \frac{e^{-jkl_2}}{l_2} \\ \frac{e^{-jkl_2}}{l_2} & s\frac{e^{-jkl_3}}{l_3} & \frac{e^{-jkl_1}}{l_1} \end{bmatrix}$$

See Takeuchi and Nelson, Acta Acustica United with Acustica Vol. 94 (2008) 981 - 987



Singular values



$$\mathbf{C} = \frac{\rho_0}{4\pi} \frac{e^{-jkl_1}}{l_1} \begin{bmatrix} 1 & se^{-jk\Delta l/2} & e^{-jk\Delta l} \\ e^{-jk\Delta l} & se^{-jk\Delta l/2} & 1 \end{bmatrix}$$

Find eigenvalues from roots of determinant of

 $\lambda I - CC^H$

Singular values given by

 $\sigma_{+} = \sqrt{[2 + 2s^{2} + 2\cos k\Delta l]}, \quad \sigma_{-} = \sqrt{[2 - 2\cos k\Delta l]}$

Optimal conditioning given by $s=\sqrt{2}$ which shows

$$\Delta l = n\lambda/2$$



Optimal source angle as a function of frequency



Optimal source angle giving perfect conditioning for $n = \pm 1, \pm 3, \pm 5$



Radiation properties of the two channel OSD



In the far field $r pprox r_1 pprox r_2$

$$\left|p(r,\phi)\right|^{2} = \left(\frac{\rho_{0}}{4\pi r_{1}}\right)^{2} \left(1 - \sin(kasin\phi)\right)$$





Radiation pattern examples

Two channel OSD at 2058 Hz



Three channel OSD at 3206 Hz





Radiation patterns as a function of source angle



Two channel OSD

Three channel OSD





Discretisation of the Optimal Source Distribution



$$\mathbf{w} = \begin{bmatrix} \mathbf{w}_A \\ \mathbf{w}_B \end{bmatrix} = \begin{bmatrix} \mathbf{A} \\ \mathbf{B} \end{bmatrix} \mathbf{v} = \mathbf{C}\mathbf{v}$$
$$\hat{\mathbf{w}}_B = \mathbf{D}\mathbf{d}$$
$$\begin{bmatrix} \hat{w}_{B1} \\ \hat{w}_{B2} \\ \hat{w}_{B3} \\ \hat{w}_{B4} \end{bmatrix} = \begin{bmatrix} 1 & 0 \\ 0 & 1 \\ 1 & 0 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} d_R \\ d_L \end{bmatrix}$$

See P.A. Nelson, T. Takeuchi, P. Couturier, X. Zhou, J. Sound Vib.539 (2022) 117259



Condition number of matrices **B** and **C** for 2Ch OSD





Condition number of matrices **B** and **C** for 3Ch OSD





Method (1) Minimise deviation from OSD sound field



$$min\left[\left\|\mathbf{A}\mathbf{v} - \hat{\mathbf{w}}_A\right\|_2^2 + \beta \left\|\mathbf{v}\right\|_2^2\right]$$

Solution given by

$$\mathbf{v}_{opt} = [\mathbf{A}^{\mathrm{H}}\mathbf{A} + \beta \mathbf{I}]^{-1}\mathbf{A}^{\mathrm{H}}\hat{\mathbf{w}}_{A}$$

Numerical experiments with 95 equispaced far field sensors

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Variation in number of sources

All results with regularisation $\beta = 0.01$

62 Sources







Source angle θ (deg)



Source angle θ (deg)

Southampton Method (2) Minimise deviation from OSD sound field with the constraint of crosstalk cancellation



$$\min \left\| \mathbf{A} \mathbf{v} - \hat{\mathbf{w}}_A \right\|_2^2$$
 subject to $\hat{\mathbf{w}}_B = \mathbf{B} \mathbf{v}$

Solution via QR decomposition given by

$$\mathbf{v}_{opt} = \mathbf{Q}_2 \mathbf{A}_2^{\dagger} \hat{\mathbf{w}}_A + (\mathbf{Q}_1 \mathbf{R}^{\mathrm{H}-1} - \mathbf{Q}_2 \mathbf{A}_2^{\dagger} \mathbf{A}_1 \mathbf{R}^{\mathrm{H}-1}) \hat{\mathbf{w}}_B$$

$$\mathbf{B}^{\mathrm{H}} = \mathbf{Q} \begin{bmatrix} \mathbf{R} \\ \mathbf{0} \end{bmatrix} \quad \mathbf{A}\mathbf{Q} = \begin{bmatrix} \mathbf{A}_1 & \mathbf{A}_2 \end{bmatrix} \quad \mathbf{Q} = \begin{bmatrix} \mathbf{Q}_1 & \mathbf{Q}_2 \end{bmatrix}$$

 $\mathbf{A}_2^\dagger = [\mathbf{A}_2^{\mathrm{H}}\mathbf{A}_2]^{-1}\mathbf{A}_2^{\mathrm{H}}$



20

-10

-20

-30

10 k

5k

2k

500

20 k

10 k

5k

2k

500

Frequency (Hz)

-90

-60

-30

-30

0

Source angle θ (deg)

0

Source angle θ (deg)

30

60

60

30

90

90

30

20

10

-10

-20

Frequency (Hz)

Results of imposing crosstalk cancellation constraint



Without regularisation

With regularisation of $\mathbf{A}_2^\dagger = [\mathbf{A}_2^{\mathrm{H}}\mathbf{A}_2]^{-1}\mathbf{A}_2^{\mathrm{H}}$

Southampton Method (3) Minimise the L2 norm of the source strength vector



$$\min \|\mathbf{v}\|_2^2$$
 subject to $\hat{\mathbf{w}}_B = \mathbf{B}\mathbf{v}$

Solution given by

$$\mathbf{v}_{opt} = \mathbf{B}^{\mathrm{H}} [\mathbf{B}\mathbf{B}^{\mathrm{H}} + \beta \mathbf{I}]^{-1} \mathbf{D}\mathbf{d}$$

See also Holleborn et al, JAES 69 (3) (2021) 191-203.



Effect of regularisation





Results of L2 norm minimisation (3Ch OSD)

Using 15 sources and 3 spaced apart listeners





Results at

1995 Hz

Southampton Method (4) Minimise the L1 norm of the source strength vector



$$min \|\mathbf{v}\|_1$$
 subject to $\hat{\mathbf{w}}_B = \mathbf{B}\mathbf{v}$

Solutions computed numerically using CVX package



Single listener crosstalk cancellation (3Ch OSD)

Frequency of 1995 Hz







Single listener crosstalk cancellation (3Ch OSD)

Results with additional symmetry constraint imposed





Single listener crosstalk cancellation (3Ch OSD)

Results with additional symmetry constraint imposed





Results for crosstalk cancellation at three spaced apart listeners

min V subject to $\hat{\mathbf{w}}_B = \mathbf{B}\mathbf{v}$ and $v_m = -v_{-m}$ 20000 15 10000 10 5000 Frequency, (Hz) [dB] 1000 -10 -15 350 -60 -40 -20 20 40 60 80 Listening angle, (deg)





The OSD in automotive applications







Conclusions

- A number of strategies for making use of the remarkable properties of the Optimal Source Distribution (OSD) have been analysed by using numerical simulations
- Replicating the OSD sound field can be achieved in principle, but requires a large number of sources
- Minimising the deviation from the OSD sound field with the constraint of crosstalk cancellation at a number of listeners seems feasible
- Minimising the L2 norm of the source strength vector appears also to give good results
- Minimising the L1 norm of the source strength vector with a symmetry constraint appears to yield the same solution as the OSD for a single listener
- Minimising the L1 norm of the source strength vector seems also to provide a sparse solution for multiple listeners



Further work

- Evaluate the subjective performance of such systems, paying particular attention to the time domain response associated with the different strategies available
- Understand better the process of L1 norm minimisation (a variety of algorithms are available some apparently simple and efficient)
- Investigate further the optimal geometrical disposition of sources and listeners and the influence of such factors on subjective performance



YOUR QUESTIONS